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ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND ABERD--ETC F/G 19/6  
BARREL EROSION RATE OF A 60MM GUN.(U)  
AUG 78 G SAMOS, B B GROLLMAN, J R WARD

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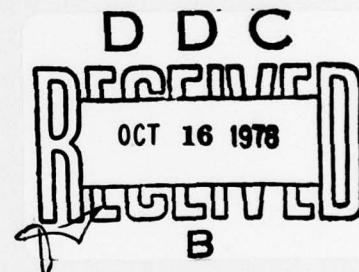
⑨ MEMORANDUM REPORT ARBRL-MR-02857

⑥ BARREL EROSION RATE OF A 60MM GUN.

⑩ George/Samos,  
Bertram B./Grollman  
J. Richard/Ward

⑪ August 1978

⑫ 5p



⑬ ARBRL-MR-02857

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20. Abstract (Cont'd)

→ In order to test the hypothesis that the various additives were not affecting the wear rate of the cannon, ten rounds were fired without any additives. The wear rate increased to 2.0 mils/rd (0.051 mm/rd). The ten round group was followed by a five round series with additive which showed the same low wear rate seen in the first 69 rounds.

The wear profile of the MC-AAAC cannon is similar to the wear profile of the 105mm M68 tank cannon firing rounds without additive. However, the MC-AAAC did not have a secondary wear peak.

The wear rate without additive was predicted reasonably well by both the Frankle and Smith-O'Brasky models. The Smith-O'Brasky model, which has a correction to the propellant flame temperature to account for the presence of the wear-reducing additive, correctly predicted the wear rate of the MC-AAAC with the additive.

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## I. INTRODUCTION

Erosion of gun tubes has long been a problem which appears to worsen as technology proceeds towards higher pressures and velocities. Various additives are currently being used to reduce erosion. In the 105mm tank cannon, for example,  $TiO_2$ /wax liners decreased the erosion rate from 0.075 inch (1.9mm) per 100 rounds to the same wear rate per 10,000 rounds<sup>1</sup>. A Canadian report<sup>2</sup> claims that polyurethane foam failed to reduce erosion in a smoothbore, high velocity gun operating with chamber pressures near 75 kpsi (517 MPa).

During the course of the Anti-Armor Automatic Cannon Technology Program (AAAC), various tests were conducted with 60mm gun tubes firing slug and APFSDS projectiles. Three different wear reducing additives were utilized in order to keep tube erosion at a minimum. Average pressures were about 80 kpsi (551 MPa), with velocities close to 5000 fps (1524 m/s). Stargage measurements of the tube showed that regardless of the type of additive used, the wear rate was 0.7 mil (0.018mm) per round. This led to speculation that the wear-reducing additives were ineffective in reducing erosion under the 60mm gun conditions. To test this hypothesis, a ten round group of slugs was fired without additive. The data from this test were also useful in determining how well existing models<sup>3,4</sup> can predict gun erosion rates.

## II. EXPERIMENTAL

The 60mm guns used in the program were fabricated by Watervliet Arsenal. Ballistic Gun 3 (BG3), the second gun used, has a total length of 226 inches (5.74 meters) and a travel of 217 inches (5.51 meters).

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1. *I. Ahmad, "The Problem of Gun Barrel Erosion, An Overview", Proceedings of Tri-Service Gun Tube Wear and Erosion Symposium, March 1977.*
2. *G. Bertrand and J.J. Maroney, "A High Performance Experimental Smooth Bore Gun 1965-1967 Coolant Trials at Chamber Pressures of 75,000 psi", Defense Research Establishment, Valcartier Technical Note 1887/70, June 1970.*
3. *J.M. Frankle and L.R. Kruse, "A Method for Estimating Service Life of a Gun or Howitzer", BRL Memorandum Report No. 1852, June 1967. (AD #818348)*
4. *C.S. Smith and J.S. O'Brasky, "A Procedure for Gun Barrel Erosion Life Estimation", Proceedings of the Tri-Service Gun Tube Wear and Erosion Symposium, March 1977.*

Rifling in the tube consists of 16 lands and grooves, with a twist of one turn in 200 calibers. The chamber configuration is shown in Figure 1. The slug projectile fired from BG3 is shown in Figure 2 and the APFSDS projectile is shown in Figure 3.

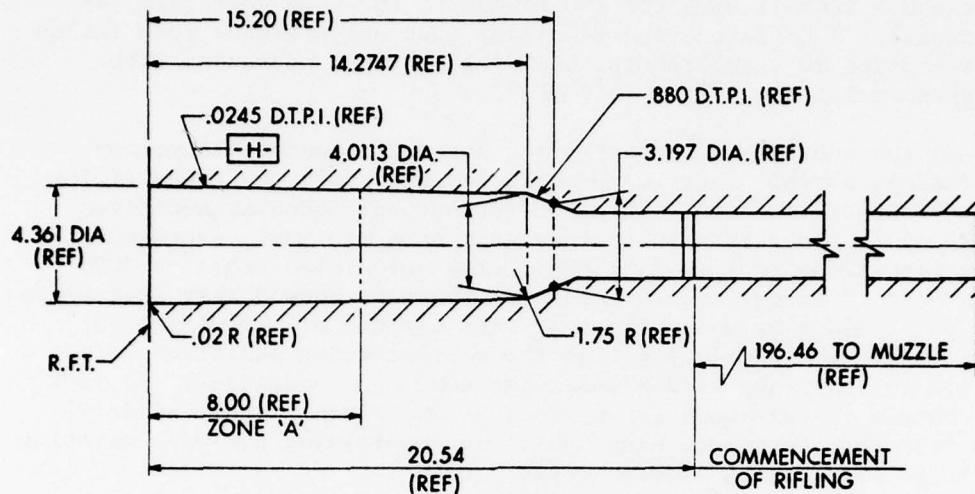


Figure 1. 60mm BG3 Chamber Configuration

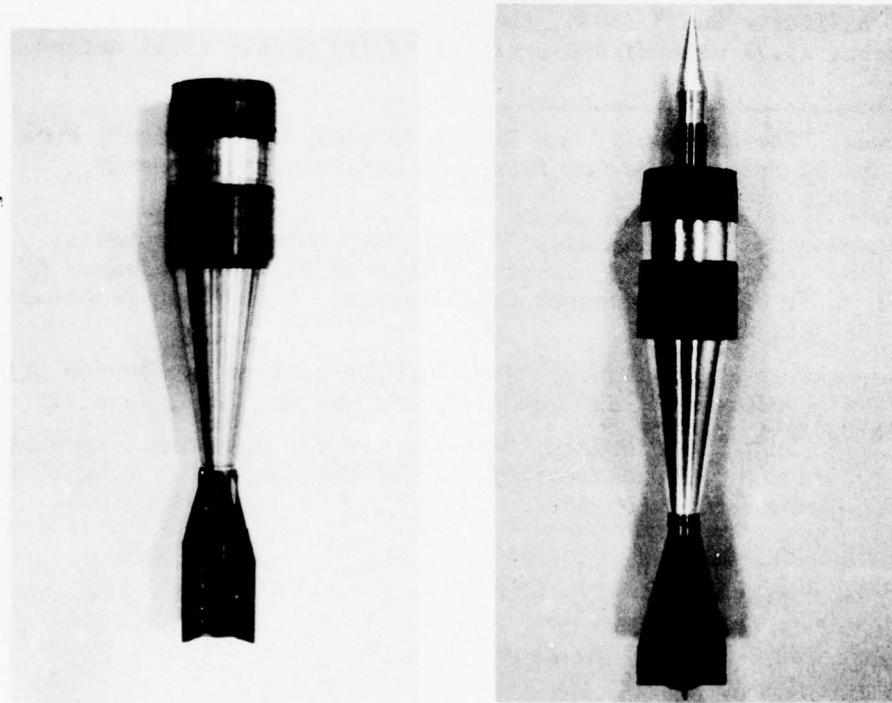


Figure 2. Standard Plug Projectile

Figure 3. APFSDS Projectile

Stub-steel cases, shown in Figure 4, were used to contain part of the propellant. The remainder of the propellant was arranged around the rear of the projectile, as shown in Figure 5. Talc/wax and  $TiO_2$ /wax additives, which are available in nominal thickness of 1/8 inch (3mm) sheet form, were wrapped around the propellant, as shown in Figure 6. The M83 electric primer and a 650 grain black powder base igniter, also shown in Figure 4, ignited the charge.



Figure 4. Stub Case, Primer and Igniter

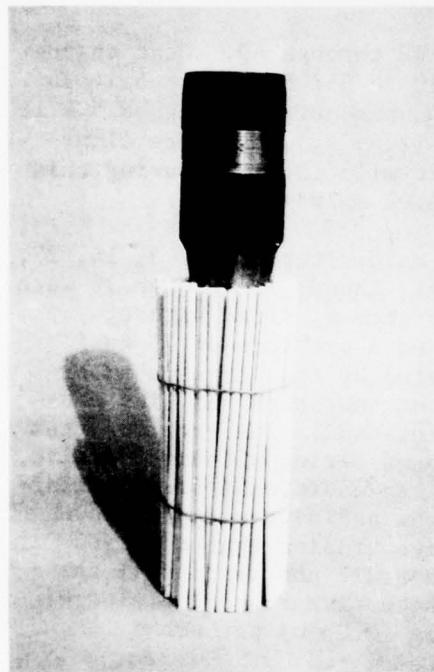


Figure 5. Propellant Sticks Arranged Around Rear of Projectile

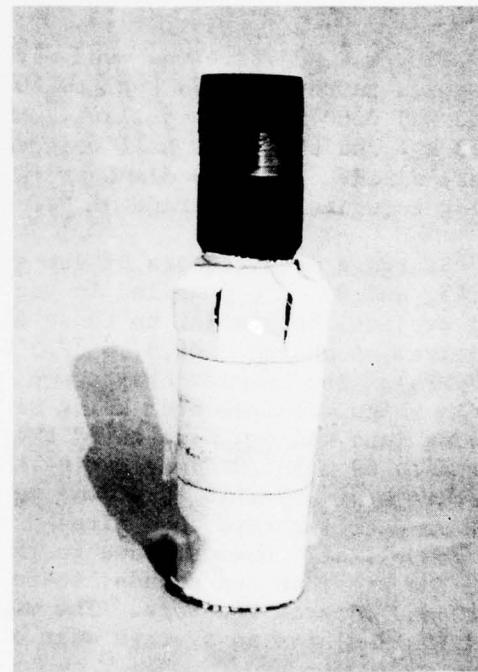


Figure 6.  $TiO_2$ /Wax Additive Wrapped Around Propellant

The M30 propellant used in the tests with BG3 were Lot No. PA-E 03795 and PA-E 03796, 0.068" web, single perf, slotted stick, and Lot No. RAD-PE 472-24, 0.078" web, single perf, slotted stick. The latter was used only in one series of firings, when a combustible case, shown in Figure 7 was used. The additive used with the combustible case was a Cabosil silicone grease placed in a plastic sleeve approximately one and one-half inches wide and 10 inches long (4 x 25cm). The sleeve was wrapped around the base of the rear band prior to loading the combustible case with the propellant sticks.

Talc/wax additive was used with the first 27 rounds fired from BG3. Peak chamber pressures ranged from 74 kpsi to 80 kpsi (510 MPa to 552 MPa), with a charge of 5.2 lb (2.36 kg). Projectile weight was 5.8 lb (2.63 kg). The vertical land diameter at 20.75 inches RFT (527.0mm) increased by 22 mils (0.56mm) corresponding to an average wear rate of 0.8 mil/rd (0.02 mm/rd).

Cabosil grease and the combustible case were used with rounds 28 through 47. 5.03 lb (2.28 kg) of 0.078" web stick propellant was used since the impetus of the combustible case was equivalent to 0.25 lb (0.11 kg) of the stick propellant. Peak chamber pressures ranged from 76 kpsi to 81 kpsi (524 to 559 MPa). Projectile weight was 5.8 lb (2.63 kg). The vertical land diameter increased by 13 mils (0.33mm) during the nineteen round group for an average wear rate of 0.7 mil/rd (0.018 mm/rd).

TiO<sub>2</sub>/wax additive was used with rounds 48 through 69. Peak chamber pressures ranged from 74 kpsi to 80 kpsi (510 to 552 MPa) with 5.14 lb (2.33 kg) 0.067" web propellant. Half of the projectiles weighed 5.8 lb (2.63 kg) and the other half weighed 5.5 lb (2.49 kg), and were alternately fired. The bore diameter increased 16 mils (0.41mm) during this firing sequence, an average of 0.8 mil/rd (0.02 mm/rd).

Stargage measurements of the gun tube, made after rounds 3, 14, 27, 34, 47, and 69, are compiled in the Appendix. Rounds 70 through 79 were slug projectiles similar to those shown in Figure 8, fired without additive. A charge of 5.5 lb (2.5 kg) yielded a pressure of 75 kpsi (517 MPa). The heavier charge was necessitated by the larger chamber volume which resulted from using slugs without the sabot and fins protruding into the chamber behind the obturating band. The bore diameter increased 19 mils (0.48mm) during the ten-round series without additive, an average of 1.9 mils (0.048mm) per round. An additional five similar slug projectiles were then fired with TiO<sub>2</sub>/wax additive wrapped around the propellant. However, due to the excessive erosion that occurred with the previous ten rounds, these five slugs did not seat until the rear band entered the bore. The wear for these five rounds totaled 6 mils (0.15mm) for an average wear of 1.2 mils (0.03mm) per round.

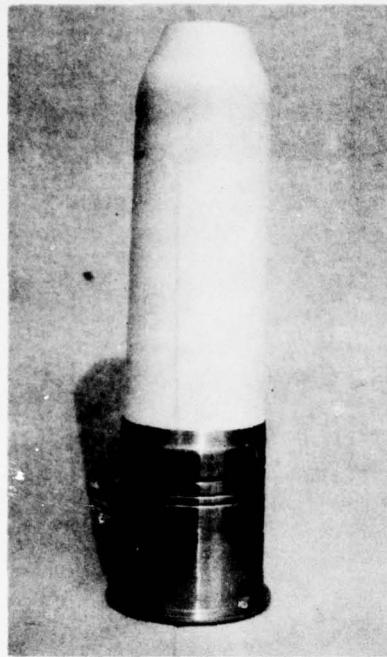


Figure 7. Combustible Case

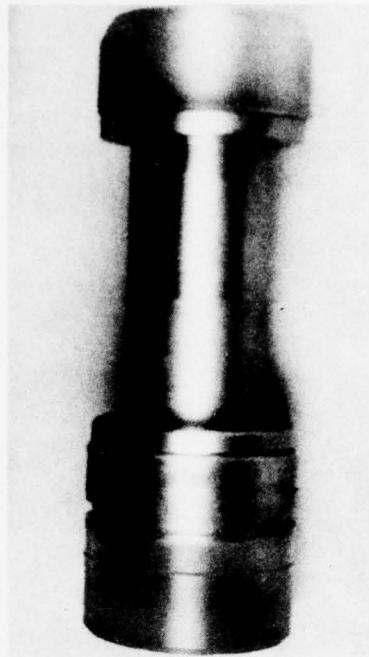


Figure 8. Slug Projectile

### III. RESULTS AND DISCUSSION

Plots of horizontal and vertical land and groove wear, measured at 20.75 inches (527mm) from the rear face of the tube (RFT), are shown in Figures 9 and 10. It is evident from the plots that the wear rate per round is linear and is the same regardless of the type of additive used. Another feature of interest is that the land wear is slightly greater than the groove wear, 0.7 mil/rd vs 0.6 mil/rd (0.018 mm/rd vs 0.015 mm/rd). The vertical lands wear slightly faster than the vertical grooves, while the grooves in the vertical and horizontal planes wear at the same rate. The datum for horizontal land wear after 34 rounds fired appears to be an erroneous stargage reading, since the wear rate of the vertical lands and both horizontal and vertical grooves after 34 rounds fell on the slope of wear/round to 69 rounds fired.

The linear wear rate for BG3 is similar to the wear pattern of the 105mm M68 gun mounted on the M60 tank. Figure 11 shows the M68 tube wear at 25.25 inches RFT (641.4mm) for APDS rounds with no additive (M392A1), with polyurethane foam (M392A2), and with  $TiO_2$ /wax additive. Of interest is that the wear rate of BG3 through 69 rounds is about the same as that of the M68 cannon firing APDS or HEAT rounds without additive. The M68 cannon is condemned after firing 100 such rounds. Assuming BG3 would be condemned at the same two percent increase in initial bore diameter, BG3 would be condemned after 60 rounds were fired.

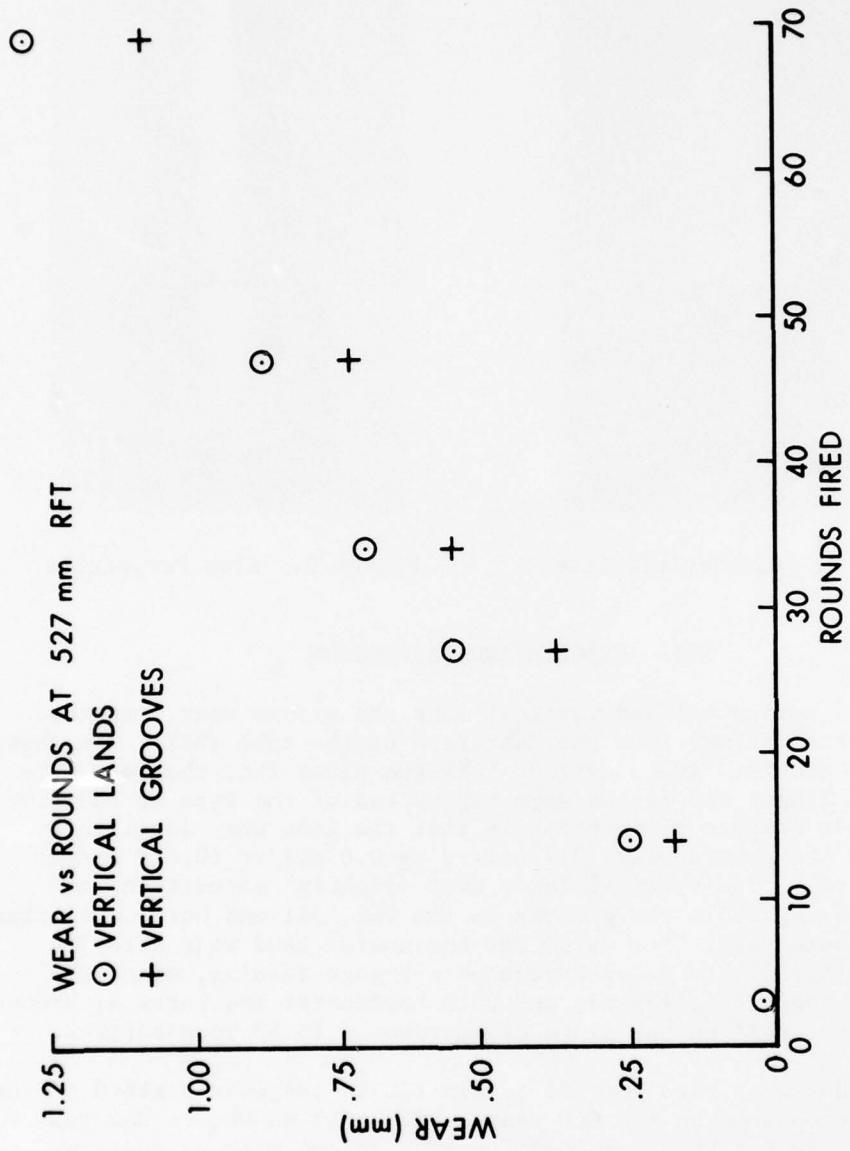


Figure 9. Vertical Groove and Land Wear vs Rounds Fired

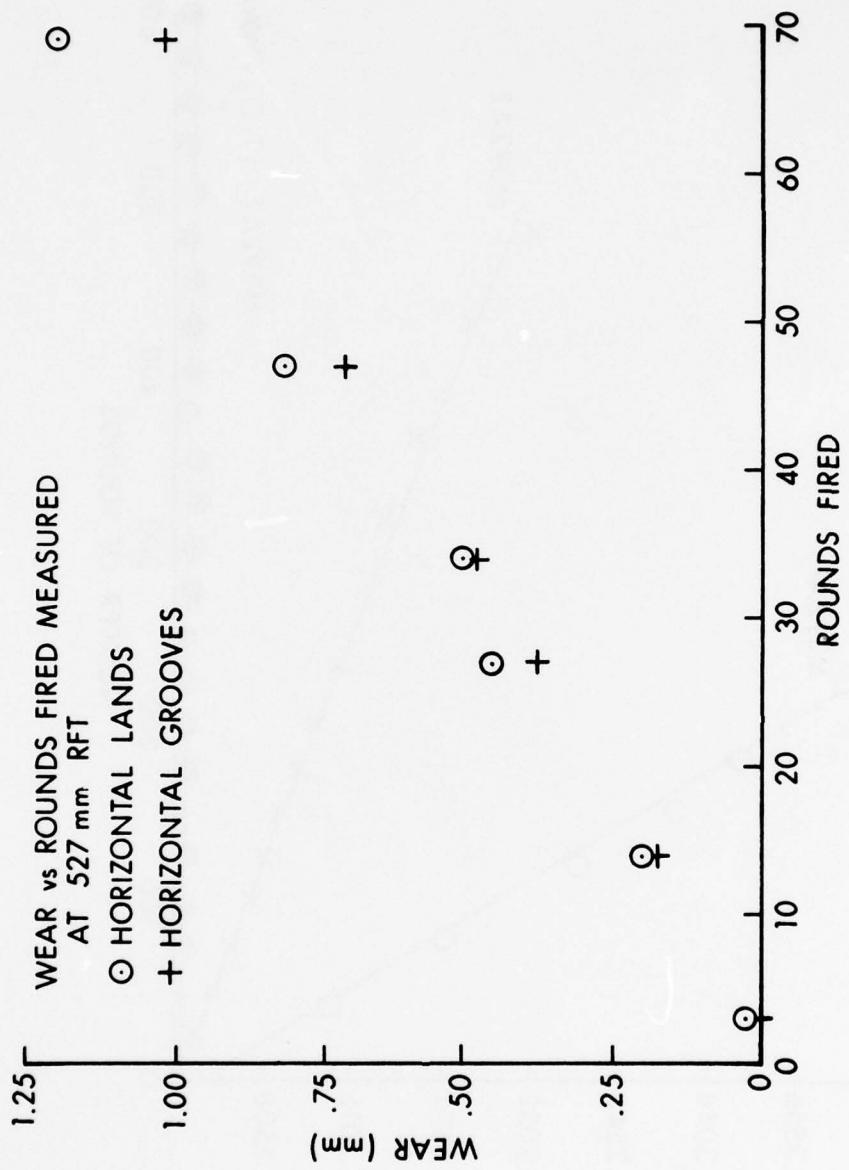


Figure 10. Horizontal Groove and Land Wear vs Rounds Fired

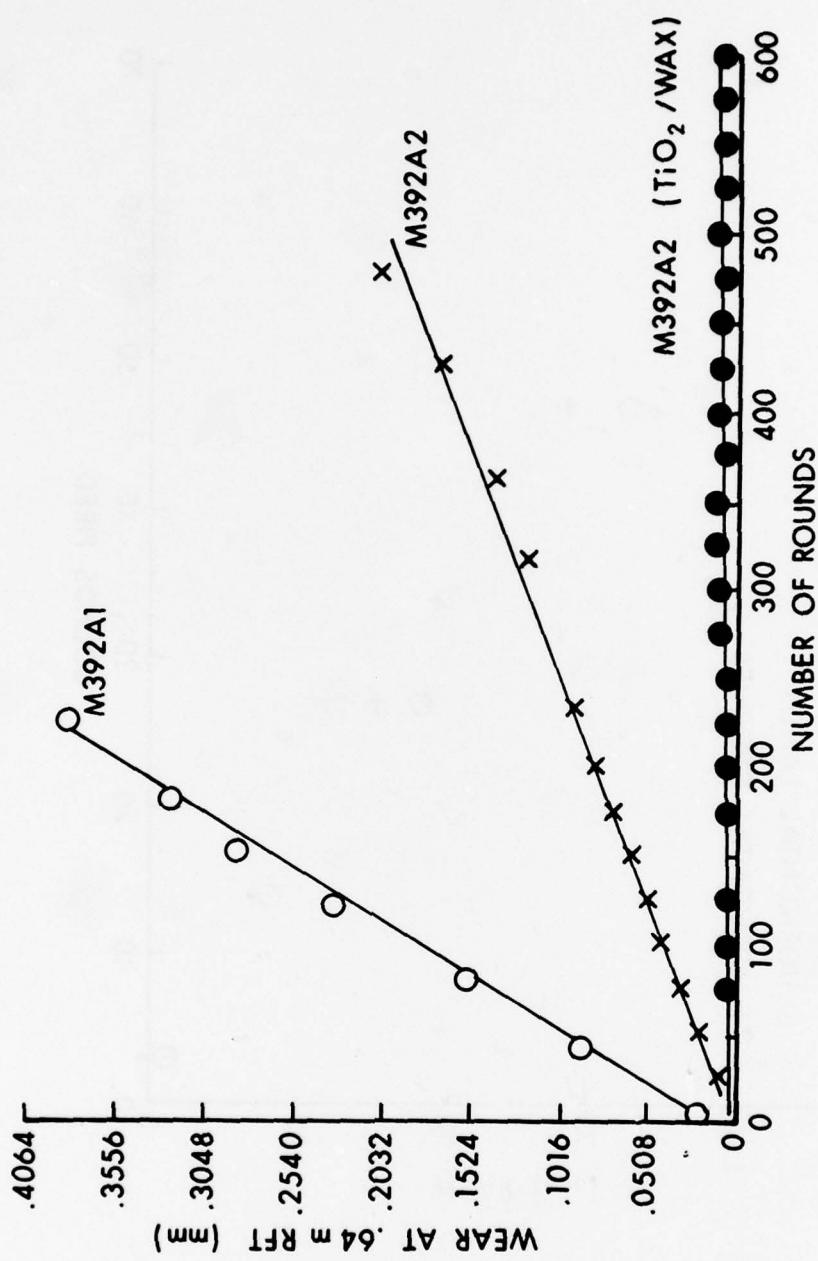


Figure 11. Vertical Land Wear for M392 Projectiles with Additives

The wear profile for BG3 after each set of stargage measurements is shown in Figure 12. This is similar to the wear profile for the M68 cannon firing rounds without additive, shown in Figure 13. However, BG3 shows no evidence of secondary wear while the M68 cannon shows secondary wear when firing rounds with polyurethane foam liners.

The bore diameter increase in BG3, after firing ten rounds (Rounds 70-79) is shown in Figure 14. Wear rate increased from 0.7 mil/round (0.018 mm/rd) to 2 mils/round (0.051 mm/rd). Both lands and grooves in the vertical and horizontal positions exhibit larger wear rates when firing rounds without additive. The bore diameter increase after firing the subsequent five rounds (Rounds 80-84) with additive is shown in Figure 15. Wear rate for these rounds dropped to the rate obtained for the first 69 rounds as illustrated in Figures 16 and 17 where only rounds fired with additive are plotted. Stargage measurement records for these two tests are also included in the Appendix.

TABLE I. Comparison Between Wear Profiles for the M392A1 and M392A2 Projectiles

RFT, cm <sup>a</sup>	M392A1 wear <sup>b</sup> mils	wear/rd <sup>4</sup> cm x 10 <sup>4</sup>	M392A2 wear <sup>c</sup> mils	wear/rd <sup>4</sup> cm x 10 <sup>4</sup>	% reduction in wear rate
64.14	123	18.	80	4.7	74
66.	83	12.	60	3.6	71
71.	80	11.	68	4.1	64
76.	70	10.	75	4.3	58
81.	60	8.6	75	4.3	50
91.	45	6.4	70	4.1	36
101.	35	5.1	63	3.8	25
112.	25	3.6	50	3.0	14
123.	16	2.	43	2.5	0
142.	10	1.5	32	1.8	0

a - distance from the rear face of the tube (RFT).

b - 177 rounds.

c - 432 rounds.

The wear profile of BG3 after firing the ten rounds without additive in contrast to the wear profile for the first 69 rounds is shown in Figure 18. To better appreciate the effect of the wear reducing additives on BG3, the wear profile is converted to the wear per round and shown in Figure 19. One sees that through 60 inches from RFT (1.52 meters) the

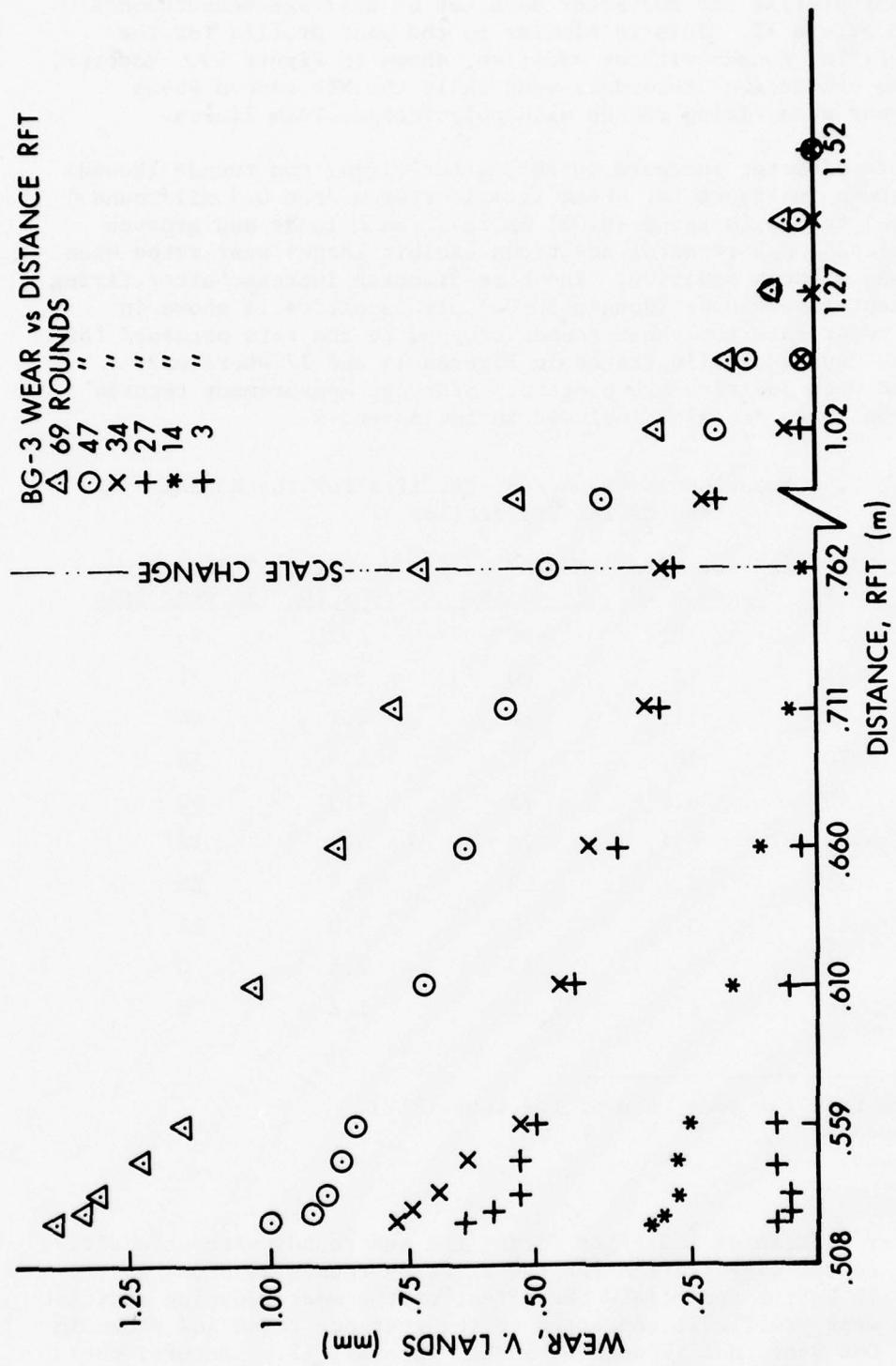


Figure 12. Tube Wear Profile for BG3

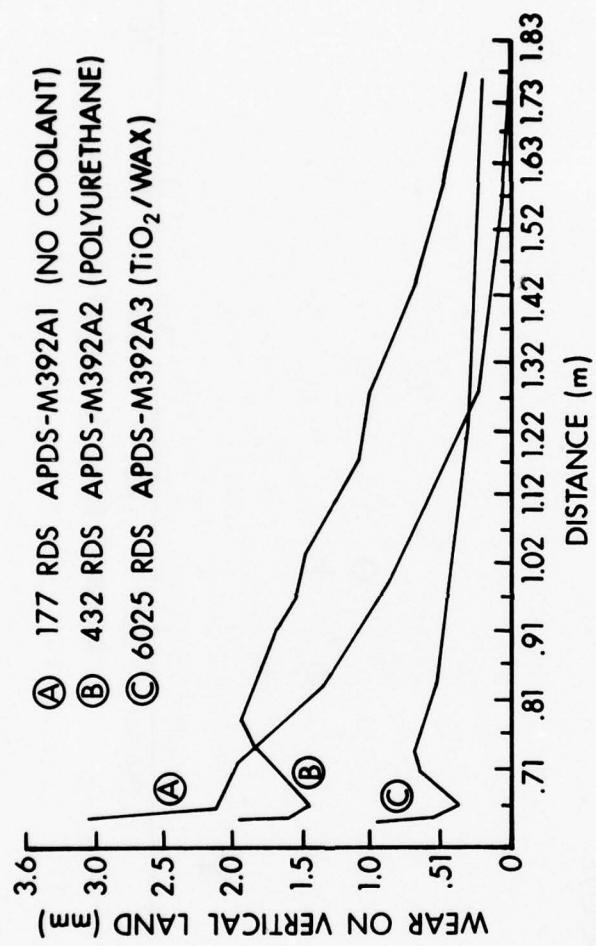


Figure 13. Tube Wear Profile for 105mm Tubes, M68

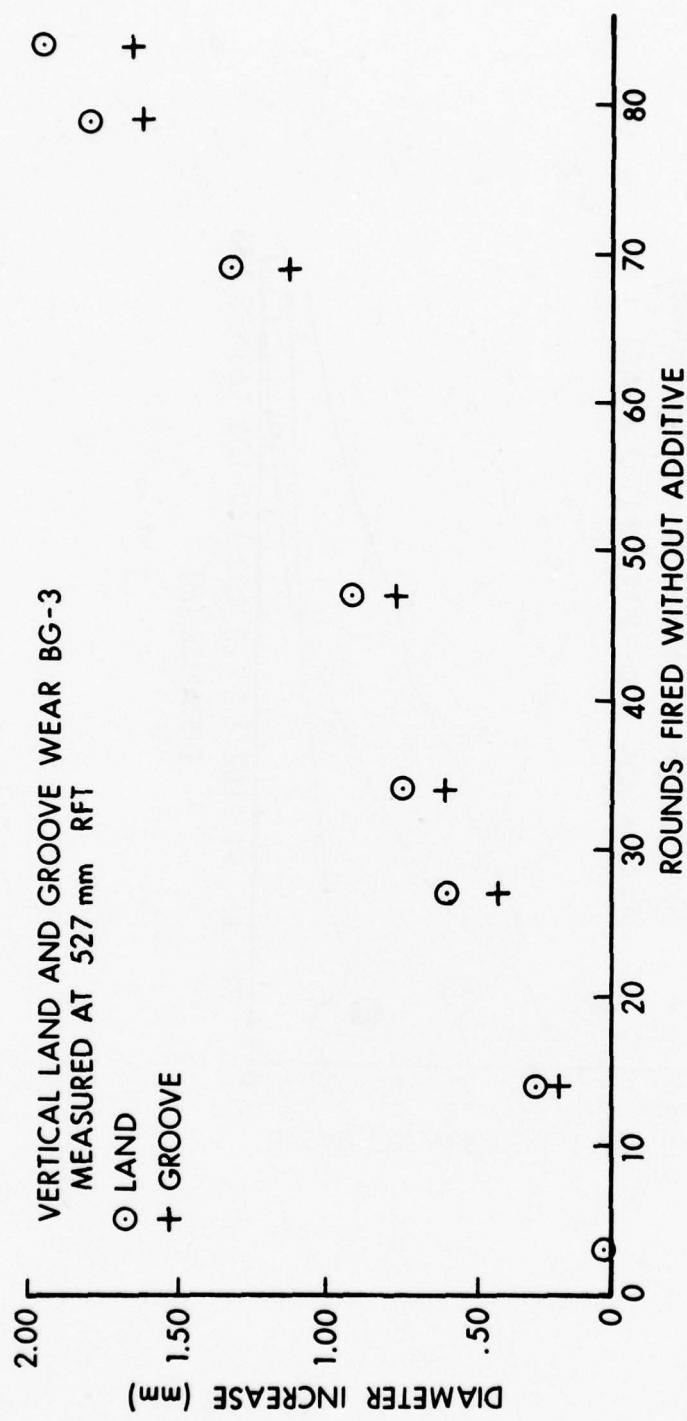


Figure 14. Vertical Land and Groove Wear for BG3 Including Rounds without Additive

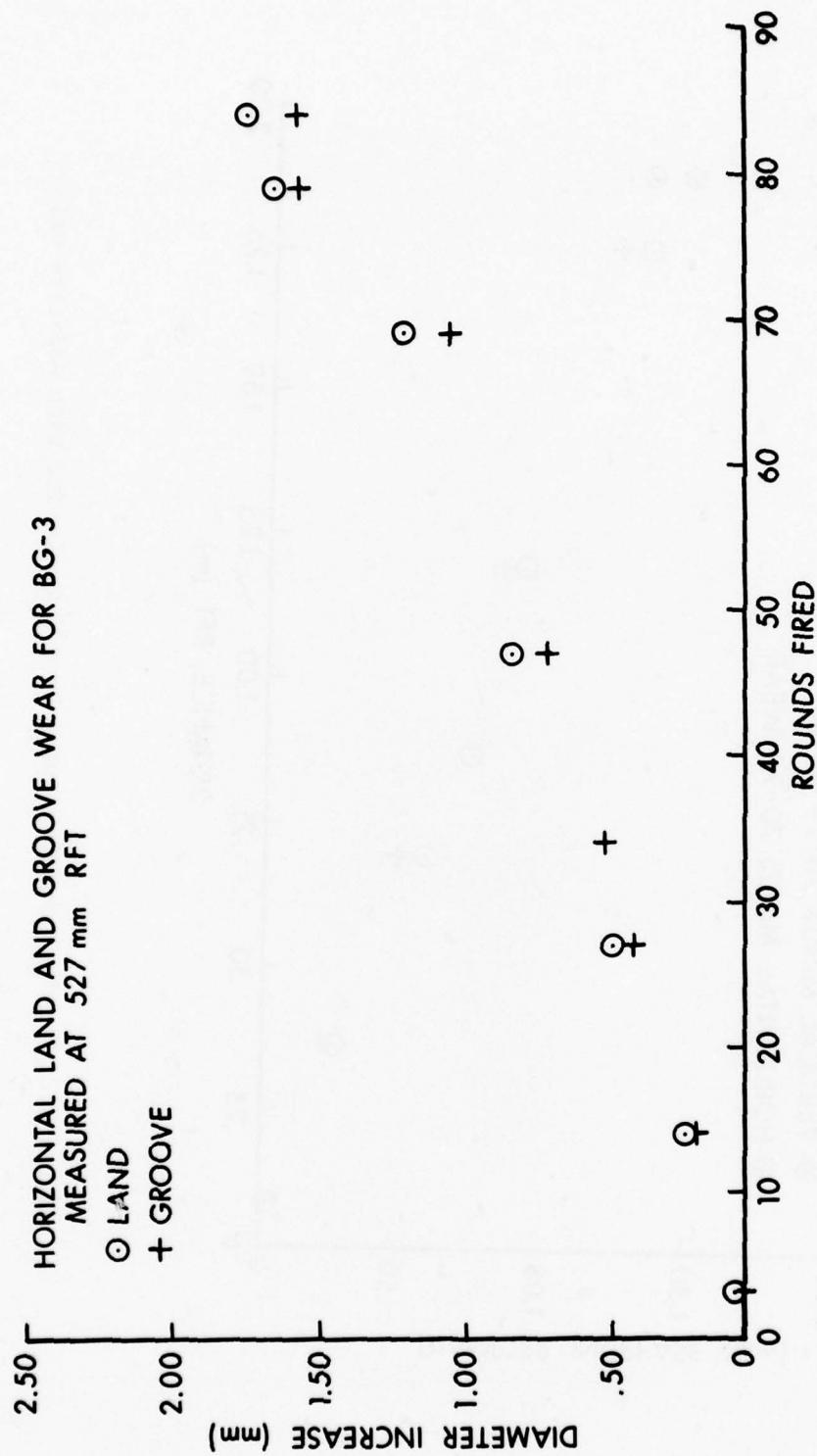


Figure 15. Horizontal Land and Groove Wear for BG3 Including Rounds without Additive

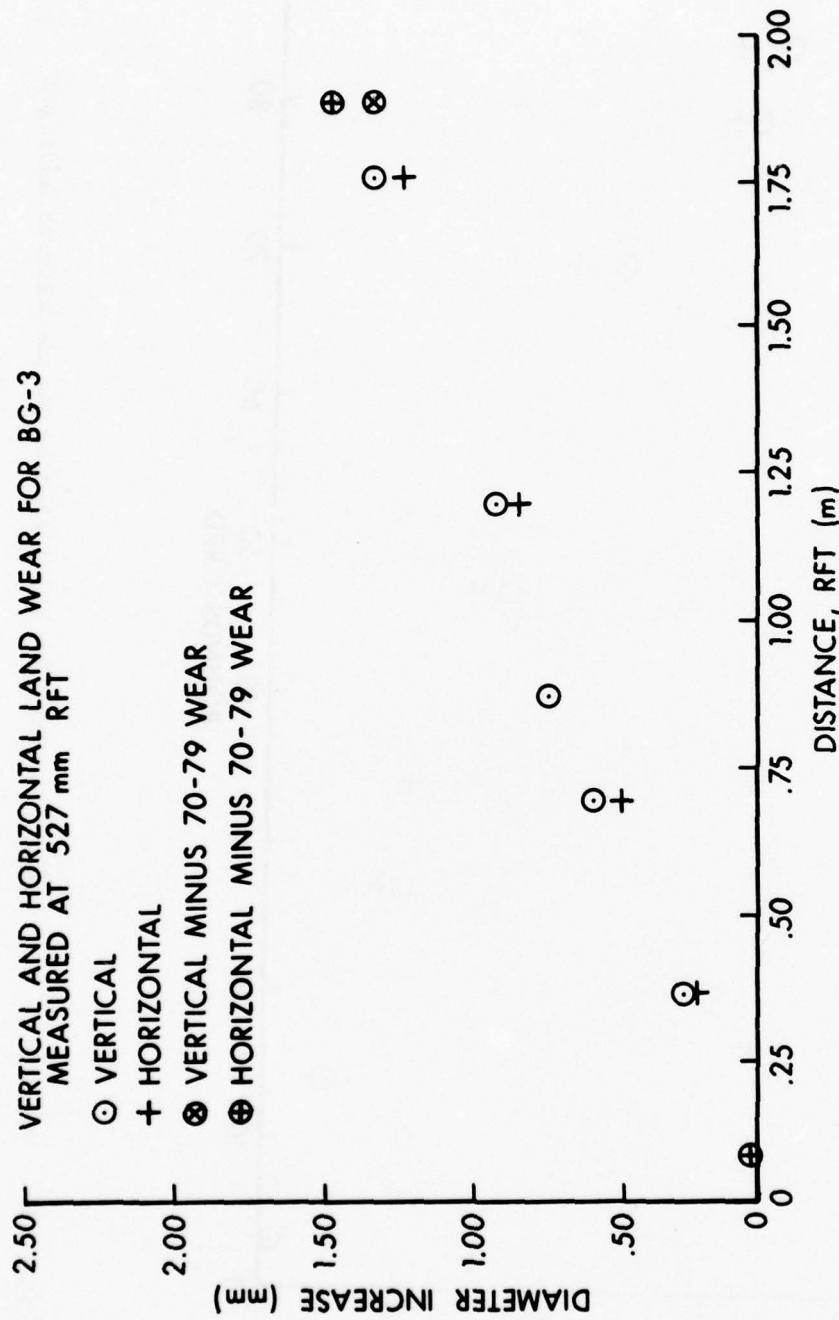


Figure 16. Vertical and Horizontal Land Wear for BG3 with Additive Only

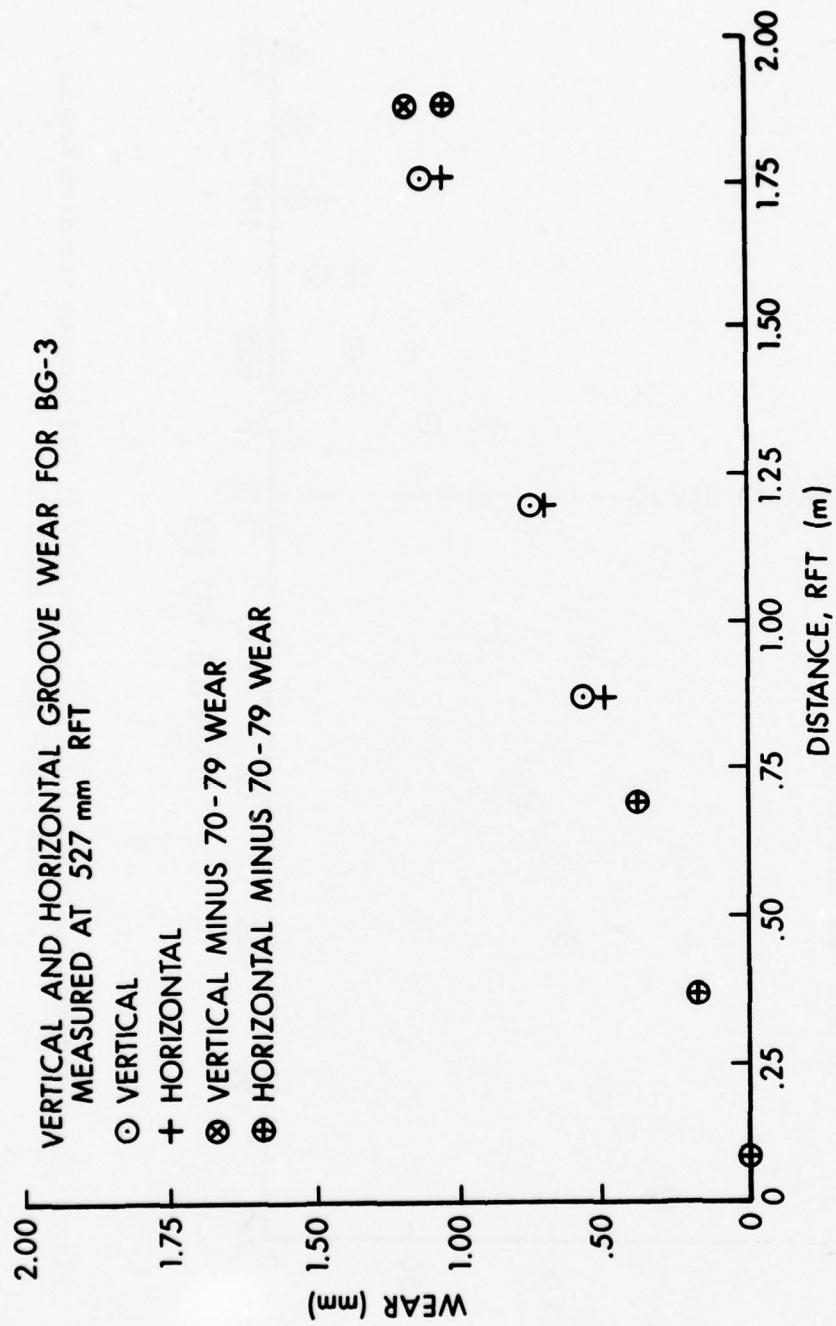


Figure 17. Vertical and Horizontal Groove Wear for BG3 with Additive Only

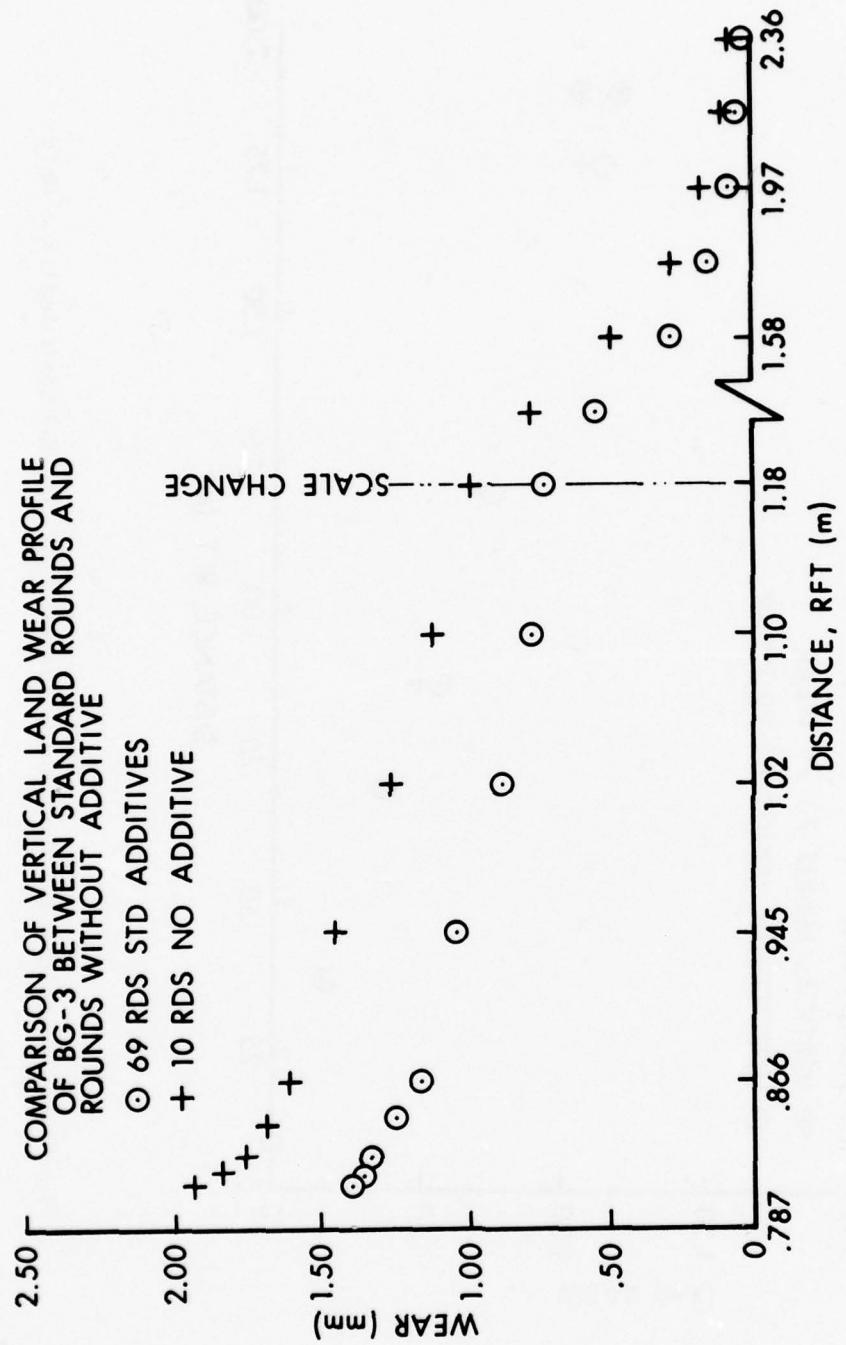


Figure 18. Comparison of Vertical Land Wear Profile of BG3 between Standard Rounds and Rounds without Additive

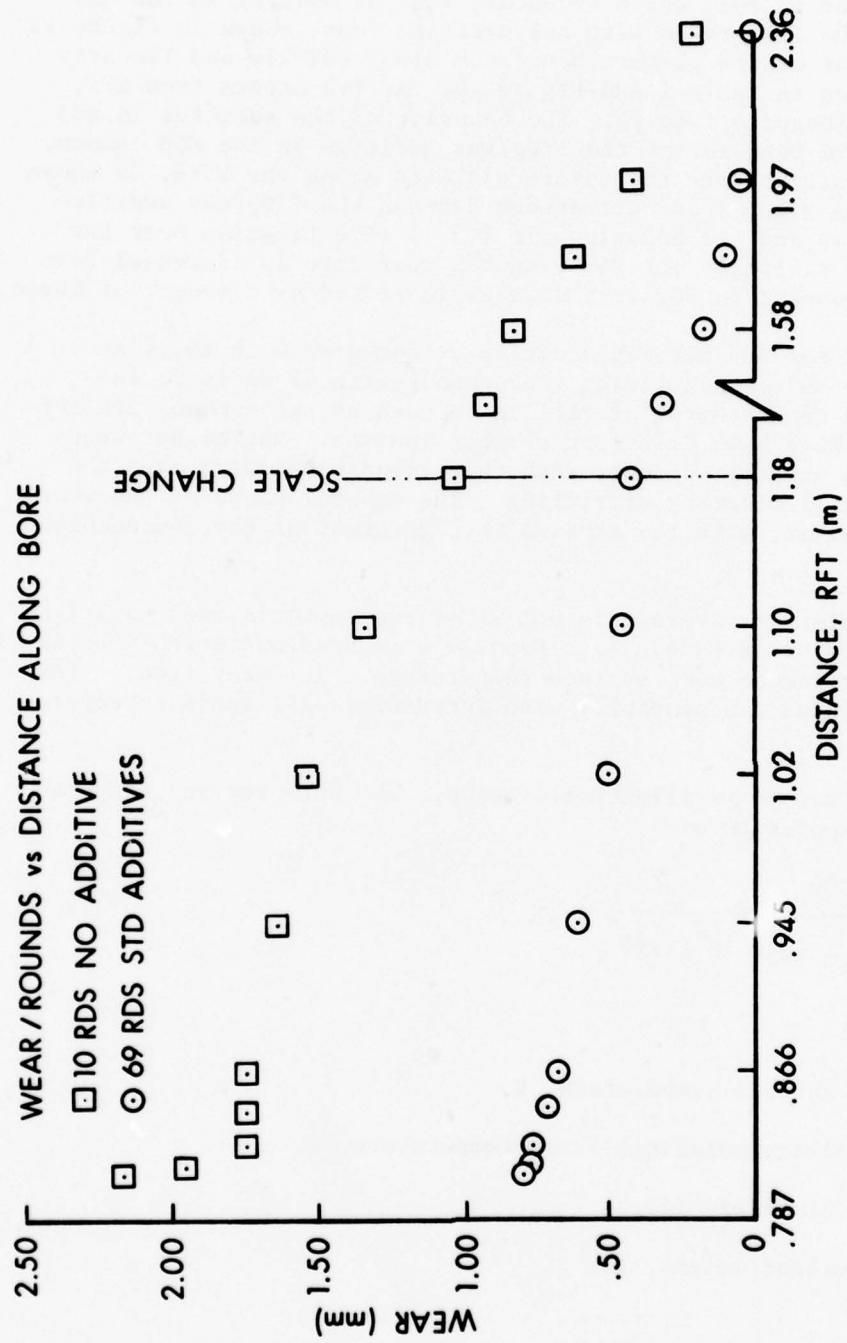


Figure 19. Wear Profile for Rounds with Additive and Rounds without Additive

additive reduces the wear of the cannon. This could explain the absence of secondary wear in BG3, while secondary wear is evident in the M68 cannon firing the APDS round with polyurethane foam, shown in Figure 13. The effectiveness of the polyurethane foam drops quickly and linearly downbore, as seen in Table I and Figure 20. At 1.2 meters from RFT, the foam is no longer effective. The behavior of the additive in BG3 is similar to the behavior of the  $TiO_2$ /wax additive in the M68 cannon, where it is effective over the entire distance along the bore, as shown in Figure 13. A significant difference between the  $TiO_2$ /wax additive in the M68 cannon and the additives in BG3 is effectiveness near the commencement of rifling. The M68 cannon's wear life is increased from 100 to 10,000 rounds; in BG3 wear life is increased by a factor of three.

Wear/round for BG3 without additive is compared with the wear profile for the M68 cannon firing APDS rounds without additive in Figure 21. The commencement of rifling is used as the common zero for the two tubes which have different chamber lengths. The higher wear rate for BG3 is clearly evident, with this trend continuing over the first 40 inches (1.0 meter) of rifling. The general shape of the wear profiles is similar, with the erosion rate greatest at the commencement of rifling.

A final point of interest is a test of two commonly used equations to compute barrel wear rate. Both Frankle's method<sup>3</sup> and Smith-O'Brasky's<sup>4</sup> model compute a pseudo bore surface temperature. The wear rate is then assumed to increase exponentially with increasing wall surface temperature.

Frankle's method is illustrated below. The bore surface temperature,  $\theta$ , is computed from

$$\theta = \frac{T_o - 300}{1.7 + 0.38d^{\frac{1}{2}} \left(\frac{d^2}{c}\right)^{.86}}, \quad (1)$$

where

$\theta$  = bore surface temperature, K,

$T_o$  = propellant adiabatic flame temperature, K,

$d$  = bore diameter, in.,

and  $c$  = propellant weight, lb.

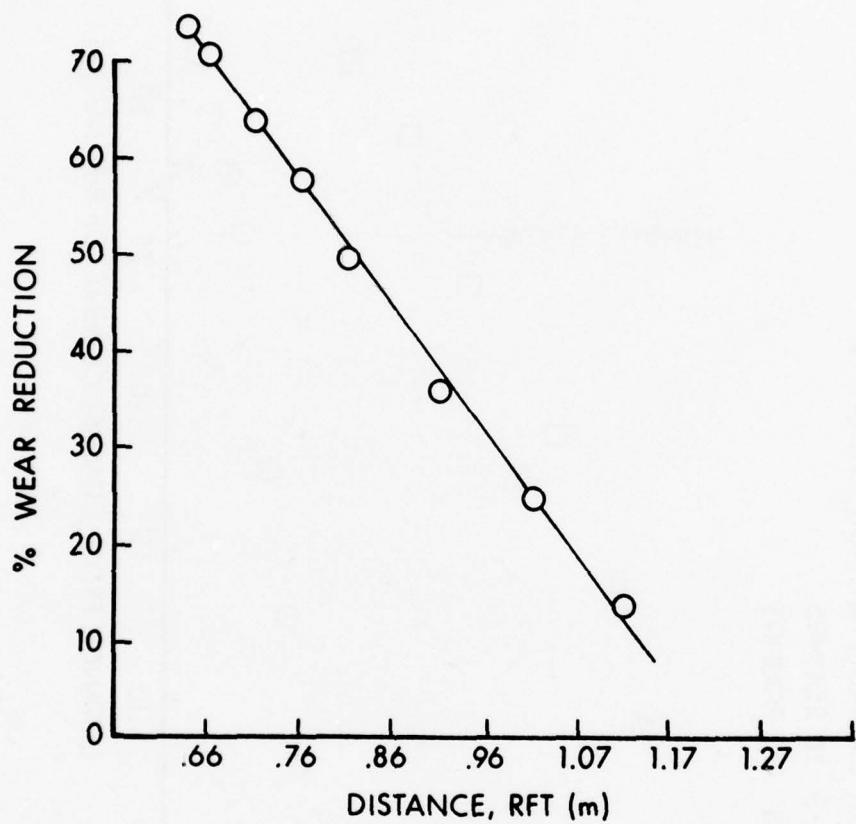


Figure 20. Wear Reduction in the M392A2 Projectile as a Function of Distance Along the Tube

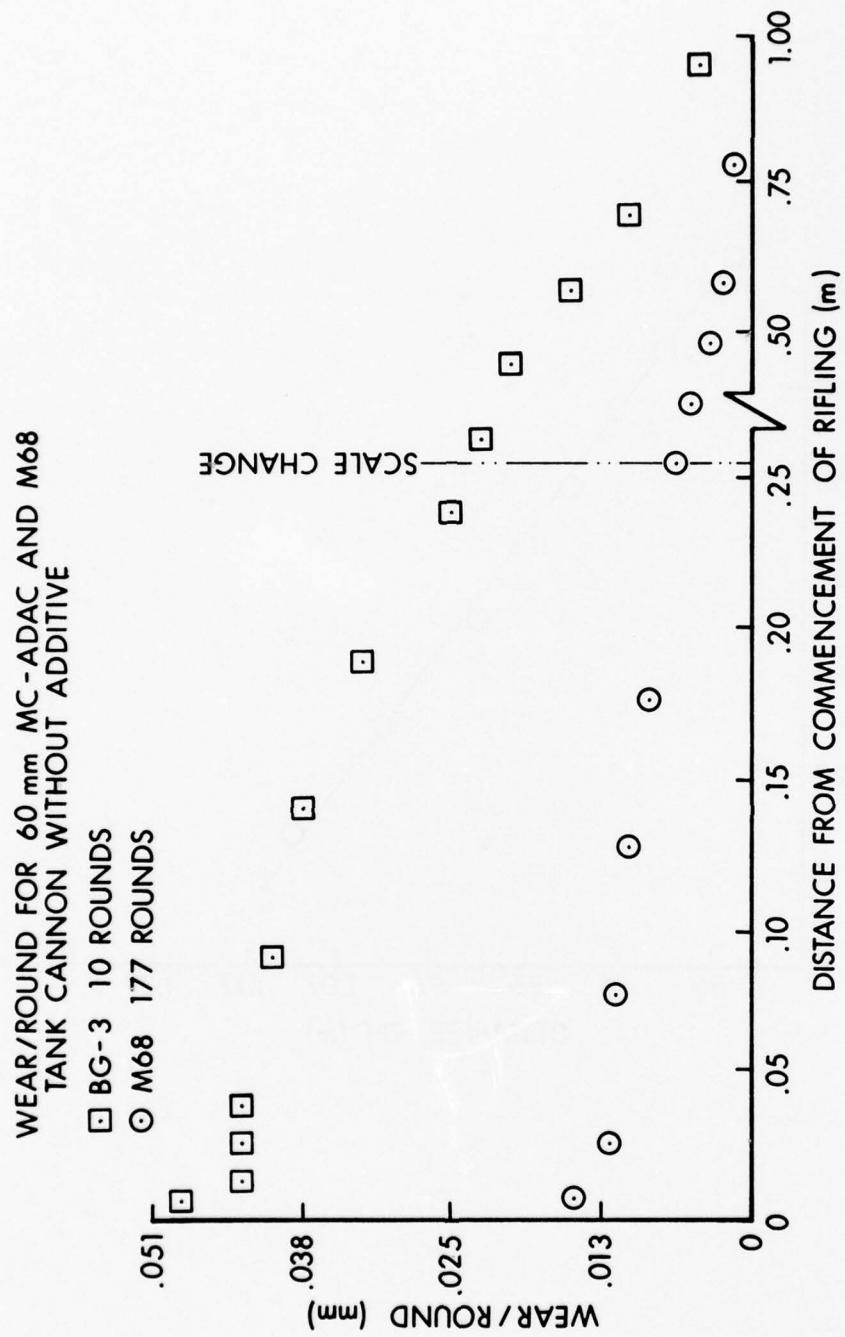


Figure 21. Wear Profile of BG3 and M68 Tank Cannon without Additive

The wear rate is then computed as follows:

$$\frac{w}{\sqrt{d}} = 8.48 \times 10^{-8} e^{.007850} \quad (2)$$

which yields the diametrical wear rate in microinches.

Smith-O'Brasky compute the wall temperature with the following expression:

$$T_w = 0.0763 \frac{T_F - T_c - 600}{d} (CP)^{\frac{1}{2}}, \quad (3)$$

where

$T_w$  = wall temperature, K,

$T_F$  = propellant flame temperature, K,

$T_c$  = effective temperature reduction by coolant, K,

d = diameter, in.,

C = charge weight, lb,

and P = peak chamber pressure, kpsi.

The wear rate in 0.1 mil per round is computed from:

$$W = 0.0166 e^{0.0049T_w} \quad (4)$$

The typical value of  $T_c$  is 500K. An expression is also available for computing wear rate during burst fire.

The predictions by each model are listed below assuming a 2.5 kg charge weight, 83,655 psi (577 MPa) peak chamber pressure, M30 propellant with a propellant flame temperature of 3040K, and  $T_c$  of 500K for the additive rounds:

<u>Model</u>	<u>Wear, mm/rd</u>	<u>Wear, mm/rd, Additive</u>
Frankle	0.038	-----
Smith-O'Brasky	.099	0.020
Experimental	.051	.018

The Frankle model predicts a wear rate closer to the experimental value, although both models predict the order of magnitude correctly for the nonadditive rounds. The Smith-O'Brasky comes remarkably close to predicting the wear rate of the rounds with additive. The Frankle method is not applicable on additive rounds. It appears, then, for the interior

ballistic parameters typical of the MC-AAAC, the empirical erosion models may be used to estimate erosion rates.

#### IV. CONCLUSIONS

1. The wear rate of BG3 without wear-reducing additives is significantly higher than the wear rate with additives. At the axial distance used to measure remaining tube life, the wear rate increased from 0.7 mil/rd (0.018 mm/rd) to 2 mils/rd (0.05 mm/rd).
2. The wear-reducing additives in BG3 exert influence on erosion over a considerable distance downbore. This is similar to the action of the  $TiO_2$ /wax liner in the M392A2 APDS projectile fired from the 105mm M68 tank cannon. However, the BG3 additives decrease the wear rate near the commencement of rifling threefold rather than the hundredfold in the M68 tank cannon.
3. The downbore wear profile of BG3 was similar to the wear profile for the M68 tank cannon firing rounds without additive. In this sense, the 60mm MC-AAAC wears in the fashion observed for other high-velocity, direct-fire cannons. In particular, the wear rate at the commencement of rifling is linear with rounds fired. In addition, no secondary wear peak is evident in the 60mm MC-AAAC.
4. Two empirical formulae for estimating tube wear rates correctly estimate the order of magnitude wear rate of BG3. The Smith-O'Brasky equation which estimates wear rate with additives also correctly estimates the wear rate of BG3 with additive.
5. If the 60mm MC-AAAC were to be condemned for the same percent increase in wear as the M68 tank cannon, BG3 would have a useful life of 60 rounds with additive and 20 rounds without additive. This suggests guns with this performance level in the 60mm caliber will require platings or coatings before they can be fielded.

#### REFERENCES

1. I. Ahmad, "The Problem of Gun Barrel Erosion, An Overview", Proceedings of Tri-Service Gun Tube Wear and Erosion Symposium, March 1977.
2. G. Bertrand and J.J. Maroney, "A High Performance Experimental Smooth Bore Gun 1965-1967 Coolant Trials at Chamber Pressures of 75,000 psi", Defense Research Establishment, Valcartier Technical Note 1887/70, June 1970.
3. J.M. Frankle and L.R. Kruse, "A Method for Estimating Service Life of a Gun or Howitzer", BRL Memorandum Report No. 1852, June 1967. (AD #818348)
4. C.S. Smith and J.S. O'Brasky, "A Procedure for Gun Barrel Erosion Life Estimation", Proceedings of the Tri-Service Gun Tube Wear and Erosion Symposium, March 1977.

APPENDIX A. STAR-GAGE MEASUREMENTS FOR BG3

## MULTIPLE STARGAGE MEASUREMENT &amp; INSPECTION DATA FORM

SHEET 1 OF 2		THIS PAGE IS BEST QUALITY PRACTICABLE PROVIDED FURNISHED TO DDC						
		60 MM Tube, MC-AAC						
NUMBER	MODEL	CASTING NUMBER	MANUFACTURER	Gauge Readings, indicated in 1/1000" or Inch				
				Front Face OF Tube	2.362" INDUS ZERO	2.362" C. CO. F. ZERO	VERT	VERT
03	MC-AAC	WVT ARS.	PROOF OFFICER W.O. 445-30601-93	216.90	+ 003	+ 001	+ 027	+ 026
				215.00	1	1	27	27
				210.00		1	27	27
				205.00		1	27	27
				200.00		1	27	27
				195.00		1	27	27
				190.00	.000	1	27	27
				185.00	0	1	27	27
				180.00	0	1	27	27
				175.35	0	1	27	27
				175.15	0	1	27	27
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				165.00	0	1	27	27
				160.00	0	1	27	27
				155.00	0	1	27	27
				150.00	0	1	27	27
				145.00	0	1	27	27
				140.00	0	1	27	27
				135.00	0	1	27	27
				130.00	0	1	27	27
				125.00	0	1	27	27
				120.00	0	1	27	27
				115.00	0	1	27	27
				110.00	0	1	27	27
				105.00	0	1	27	27
				100.00	0	1	27	27
				95.00	0	1	27	27
				90.00	0	.000	27	27
				85.00	0	0	27	27
				80.00	0	0	27	27
				75.00	0	0	27	27
				70.00	+ .001	0	27	27
				65.00	1	0	27	27
				60.00	1	0	27	27
				55.00	1	0	27	27
				50.00	1	0	27	27
				45.00	1	0	27	27
				40.00	1	+ .001	27	27
				35.00	1	1	27	27
				30.00	1	1	27	27
				28.00	1	1	27	27
				26.00	1	1	27	27
				24.00	1	1	27	27
				22.00	1	1	27	27
				21.50	1	1	27	27
				21.00	1	1	27	27
				20.75	1	1	27	27
				20.60	+ .001	+ .001	+ .027	+ .027

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SAFETY 2016

160MM MC-AAAC, TUBE #03  
22 MAR 76 BEFORE FIRE AT APC

FOR: MR SAMOS  
LNO. 445-30601-93

60 MM Tube "C" - APC					CHART						
DISTANCE (Inches) FROM					GAUGE MEASUREMENTS INDICATED IN 1/1000 OF AN INCH						
REAR FACE OF BREECH	MUZZLE FACE	REAR FACE OF TUBE	BASIC DIAMETER	ZERO	GAUGE READING	ACTUAL DIAMETER	DIFFERENCE	GAUGE READING	ACTUAL DIAMETER	DIFFERENCE	
					2.393			2.393			
		20.05			2.400			2.400			
		19.00			2.413			2.413			
		17.00			2.427			2.425			
		16.20									
		14.00			4.020			4.020			
		12.00			4.070			4.070			
		10.00			4.118			4.119			
		8.00			4.166			4.167			
		6.00			4.216			4.217			
		4.00			4.266			4.266			
		2.00			4.315			4.316			
		1.00			4.340			4.340			
		.50			4.352			4.352			
		.10			4.362			4.363			
Borescoped: (Not chrome plated)					Numerous light scratches with light stains and other deposits thru-out chamber and centering cylinder. The eccentricity of the origin of rifling in the 3:30 o'clock area measured 19.75" from rear face of tube (RFT), and in the 9:00 0' clock area measured 20.30" from (RFT); therefore the eccentricity of the origin of rifling is considered to be elongated. Several light scratches with light stains and other deposits thru-out bore. Four piezo gage holes were noted drilled through tube wall. One 60.55" from (RFT) in the 11:45 o'clock area, one 99.50" from (RFT) in the 7:00 o'clock area, one 148.25" from (RFT) in the 7:00 o'clock area, and one 200.50" from (RFT) in the 7:00 o'clock area. Appearance of no separation at the junction of tube and extension. Photos taken of origin of rifling (general view), 12:00 and 6:00 o'clock (direct shots) and a (general view) of the junction (tube and extensions).						
SPECIAL MEASUREMENTS											
TOTAL LENGTH OF GUN		BASIC	ACTUAL	ROTATION OF TUBE AT BREECH		BASIC	ACTUAL				
		—	226.00			—	—				
TOTAL LENGTH OF TUBE		—	217.00"	MOVEMENT OF TUBE AT BREECH		—	—				
DEPTH OF BREECH RECESS		—	9.00"	NUMBER OF LANDS AND GROOVES		—	16				
Inspection Remarks ( Main Bore 20.50" to 175.00", Extension 175.00 to 217.00" )											
STAMPED		STARGAUGED AND INSPECTED BY Rowman C. Crabb D.				REVIEWED BY					
RODMAN CRABB D.		TIME —				COMPIULATOR					
RECORDER T. TILDON M.		PLACE 525				GRAPHED BY					

## MULTIPLE STARGAGE MEASUREMENT &amp; INSPECTION DATA FORM

SHEET 1 OF 2		60 M/M Tube, MC-AAC			
60M/M TUBE	NUMBER	MODEL	MANUFACTURER	CASTING NUMBER	GAUGE REPS. INDICATED IN 1/1000" OF INCH
60M/M TUBE	Q3	MC-AAC	WVT. ARS		2.326" 21.800
DATE OF GAUGING	4 MAY 76	NUMBER OF ROUNDS	3	PROOF OFFICER M.R. BOYER	2.362" 21.800
DATE OF FIRING	4 MAY 76	NUMBER OF ROUNDS	3	W.O. 445-7677-94	VERT HOP VERT HOP
FIRING STATUS (Check One)	BEFORE <input checked="" type="checkbox"/> AFTER				.000 + .025 + .025
1	216.90	.000	.000		25 25
2	215.00	-.001	-.001		25 25
3	210.00				25 25
4	205.00				25 25
5	200.00				25 25
6	195.00				25 25
7	190.00				25 25
8	185.00				25 25
9	180.00				25 25
10	Junction →	175.35			25 25
11		175.15			25 25
12		170.00			25 25
13		165.00			25 25
14		160.00			25 25
15		155.00	.000		25 25
16		150.00	000		25 25
17		145.00	000		25 25
18		140.00	000		25 25
19		135.00	000		25 25
20		130.00	00		25 25
21		125.00	00		25 25
22		120.00	-.001		25 24
23		115.00			25 24
24		110.00			25 24
25		105.00			25 24
26		100.00			25 25
27		95.00			25 25
28		90.00		.000	25 25
29		85.00		00	25 25
30		80.00	.000	00	25 25
31		75.00	000	00	25 25
32		70.00	000	000	25 25
33		65.00	00	000	25 25
34		60.00	00	0000	25 25
35		55.00	00	00000	25 25
36		50.00	00	000000	25 25
37		45.00	00000	000000	25 25
38		40.00	00000	000000	25 25
39		35.00	00000	000000	25 25
40		30.00	00000	000000	27 27
41		28.00	00000	000000	27 27
42		26.00	+.001	+.001	27 27
43		24.00	2	1	27 28
44		22.00	3	2	28 28
45		21.50	3	2	28 27
46		21.00	2	2	28 27
47		20.75	2	2	27 27
48		20.60	+.003	+.002	+.026 +.027

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SHEET 2 OF 2

60 MM Tube MC-AAAC					CHAMBER					
DISTANCE (Inches) FROM					GAUGE MEASUREMENTS INDICATED IN 1/1000 OF AN INCH					
REAR FACE OF BREECH	MUZZLE FACE	REAR FACE OF TUBE	BASIC DIAMETER	ZERO	GAUGE READING	ACTUAL DIAMETER	DIFFERENCE	GAUGE READING	ACTUAL DIAMETER	DIFFERENCE
					2.382			2.382		
					2.402			2.402		
					2.415			2.414		
					2.425			2.425		
					4.020			4.020		
					4.070			4.070		
					4.118			4.119		
					4.166			4.167		
					4.216			4.217		
					4.266			4.266		
					4.315			4.316		
					4.340			4.340		
					4.352			4.352		
					4.362			4.363		
Borescoped: (not chrome plated)					Numerous light scratches with light carbon and other deposits thru-out chamber. Two score marks were noted in chamber. One in the 4:00 o'clock area between 1" to 2.5" from rear face of tube (RFT) and one in the 8:00 o'clock area between 2" to 2.75" from (RFT). The eccentricity of the origin of rifling in the 3:30 o'clock area measured 19.75" from rear face of tube (RFT), and in the 9:00 o'clock area measured 20.30" from (RFT); therefore the eccentricity of the origin of rifling is considered to be elongated. Several light scratches with light stains and other deposits thru-out bore. Four piezo gauge holes were noted drilled through tube wall. One 60.55" from (RFT) in the 11:45 o'clock area, one 99.50" from (RFT) in the 7:00 o'clock area, one 148.25" from (RFT) in the 7:00 o'clock area, and one 200.50" from (RFT) in the 7:00 o'clock area. Appearance of no separation at the junction of tube and extension. Impression taken of the two score marks in chamber. No photos taken at this time.					
SPECIAL MEASUREMENTS										
TOTAL LENGTH OF GUN	BASIC	ACTUAL	ROTATION OF TUBE AT BREECH			BASIC	ACTUAL			
	—	226.00"				—	—			
	—	217.00"				—	—			
DEPTH OF BREECH RECESS	—	9.00"	MOVEMENT OF TUBE AT BREECH			—	—			
			NUMBER OF LANDS AND GROOVES			—	16			
STAMPED										
RODMAN SEARS		STARGAUGED AND INSPECTED BY POWERS			REVIEWED BY					
RECORDED SCARBOROUGH		TIME —			COMPILATOR					
		PLACE TRANSONIC RANGE			GRAPHED BY					

40' O/N/M, MC-AAAC, TUBE #

MAY 76 AF 3 RDS.

TOP. 3 R. 45-17677-94

**MULTIPLE STARGASSE MEASUREMENT & INSPECTION DATA FORM**

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60 MM Tube "C" GUN					Cylinder					
DISTANCE (Inches) FROM REAR FACE OF BREECH					GAUGE MEASUREMENTS INDICATED IN 1/1000 OF AN INCH					
REAR FACE OF BREECH	MUZZLE FACE	REAR FACE OF TUBE	BASIC DIAMETER	ZERO	GAUGE READING	ACTUAL DIAMETER	DIFFERENCE	GAUGE READING	ACTUAL DIAMETER	DIFFERENCE
			20.05	2.392	2.402			2.404		
			19.00		2.411			2.412		
			17.00		2.426			2.427		
			16.20		2.443			2.443		
			14.00	4.200	4.020			4.020		
			12.00		4.069			4.070		
			10.00		4.118			4.118		
			8.00		4.166			4.167		
			6.00		4.216			4.217		
			4.00		4.264			4.266		
			2.00		4.314			4.315		
			1.00		4.340			4.340		
			.50		4.352			4.352		
			.10		4.362			4.362		
BORESCOPED: (Not chrome plated) Light scratches, stains, and deposits throughout chamber. Light smooth erosion encircling centering cylinder beginning 16.10" from rear face of tube (RFT) and continuing forward into main bore to 33" from (RFT). Lands are rounded throughout eroded area of bore with edges of lands rounded as far forward as 60" from (RFT). Light heat checking on lands and in grooves between forcing cone and 4.5" from (RFT). Heavy powder fouling and other deposits throughout bore. No noticeable erosion around piezo gauge holes. No separation at the junction of the tube and extension was noted. Casts were made of the score marks at 4:00 o'clock and 8:00 o'clock in the chamber. No photographs taken at this time.										
SPECIAL MEASUREMENTS										
TOTAL LENGTH OF GUN		BASIC	ACTUAL	ROTATION OF TUBE AT BREECH		BASIC	ACTUAL			
		—	226.00			—	—			
TOTAL LENGTH OF TUBE		—	217.00	MOVEMENT OF TUBE AT BREECH		—	—			
DEPTH OF BREECH RECESS		—	9.00	NUMBER OF LANDS AND GROOVES		—	16			
NOT STAMPED ROOMAN McWILLIAMS RECORDER SCARBOROUGH										
STARGAUGED AND INSPECTED BY		REVIEWED BY		TIME		COMPIULATOR		GRAPHED BY		
TESCH										
STEAP-DS Form 106, 17 Jun 64 (Part II)										

12 MAY 76  
60 MM, MC-MAAC, TUBE #03  
AF 14 RDS

FOR: M. J. Mayer  
W.O. II, U-77677-94

## MULTIPLE STARGAGE MEASUREMENT &amp; INSPECTION DATA FORM

NUMBER	MODEL	MANUFACTURER	CASTING NUMBER	Front Face		Rear Face		Front Face of Tube	Rear Face of Tube
				UP	DOWN	UP	DOWN		
6091mTUBE	03	MC-AAAAC	WVT-ARS.						
DATE OF GAUGING	18 MAY 1976	FIRING STATUS (Check One)	NUMBER OF ROUNDS	PROOF OFFICER M.R. BOYER W.O. 1145-77677-947		Junction			
BEFORE	AFTER		27						
1.10	210.20	+ .001	+ .001	+ .026	+ .026				
2.10	210.10								
7.00	210.00								
12.00	205.00	.000	.000						
17.00	200.00								
22.00	195.00								
27.00	190.00								
32.00	185.00								
37.00	180.00								
41.65	175.35								
41.85	175.15								
47.00	170.00								
52.00	165.00								
57.00	160.00								
62.00	155.00								
67.00	150.00								
72.00	145.00								
77.00	140.00	+ .001	+ .001						
82.00	135.00								
87.00	130.00	.000	.000						
92.00	125.00								
97.00	120.00								
102.00	115.00								
107.00	110.00								
112.00	105.00								
117.00	100.00								
122.00	95.00								
127.00	90.00								
132.00	85.00								
137.00	80.00								
142.00	75.00								
147.00	70.00								
152.00	65.00	+ .001							
157.00	60.00								
162.00	55.00								
167.00	50.00								
172.00	5.00								
177.00	10.00			+ .002					
182.00	35.00								
187.00	30.00								
189.00	28.00								
191.00	26.00								
193.00	24.00								
195.00	22.00								
195.50	21.50								
196.00	21.00								
196.25	20.75								
196.40	20.60	+ .023	+ .020	+ .042	+ .042				

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### THE STATE.

STEAP-DS Form 106, 17 Jun 64 (Part II)

40

## MULTI-PIPE STARGEAGE MEASUREMENT & INSPECTION DATA FORM

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2001 2 01 2

Gauge Measurements Indicated in 1/1000 of an Inch							
Distance (Inches) from		Gauge Measurements Indicated in 1/1000 of an Inch					
Front Face of Breech	Muzzle Face	Vertical	Horizontal				
of Breech	of Tube	Gauge Reading	Actual Diameter	Difference	Gauge Reading	Actual Diameter	Difference
ZERO				ZERO			
196.95	20.05	+0.019	2.411		+0.023	2.415	
198.00	19.00	28	.420		32	.424	
200.00	17.00	44	.436		47	.439	
200.80	16.20	+0.064	2.456		+0.064	2.456	
2.300" 2.200"				2.300" 2.200"			
202.00	14.00	-182	4.018		-181	4.019	
205.00	12.00	132	.068		132	.068	
207.00	10.00	82	.118		82	.118	
209.00	8.00	34	.164		34	.164	
211.00	6.00	+0.016	.216		+0.016	.216	
213.00	4.00	64	.264		65	.265	
215.00	2.00	113	.313		114	.314	
216.00	1.00	137	.337		138	.338	
216.50	.50	149	.349		149	.349	
216.90	.10	+.161	4.361		+.161	4.361	
SPECIAL MEASUREMENTS							
TOTAL LENGTH OF GUN		BASIC	ACTUAL	ROTATION OF TUBE AT BREECH		BASIC	ACTUAL
		-----	226.00"			-----	-----
TOTAL LENGTH OF TUBE		-----	217.00"	MOVEMENT OF TUBE AT BREECH		-----	-----
DEPTH OF BREECH RECESS		-----	9.00"	NUMBER OF LANDS AND GROOVES		16	16
Borescoped: (Not chrome plated) Light scratches, stains, and deposits thru-out chamber. Light smooth erosion encircling centering cylinder beginning 16.10" from rear face of tube (RFT) and continuing forward into main bore to 38" from (RFT). Lands are rounded thru-out eroded area of bore with edges of lands rounded as far forward as 85" from (RFT). Very light longitudinal scoring between 16.10" and 26" from (RFT). Light heat checking encircling bore between 14" and 65" from (RFT). No noticeable erosion around piezo gauge holes. No separation at the junction of the tube and extension was noted.							
No photos or impressions taken at this time.							
STAMPED STARGAUGED AND INSPECTED BY RODMAN SEARS ESCH							
TIME — COMPILATOR							
RECORDED SCARBOROUGH PLACE TRANSONIC RANGE GRAPHED BY							

60 MM MC-AAC TUBE #02  
20 OCT 76 AF WF RDS  
FOR: K.R. OSE  
W.O. F. J. U. - 776772-94  
+12-27-65

## MULTIPLE STAR GAS MEASUREMENT & INSPECTION DATA FORM

60MM Tube		DATE OF GAUGING 19 Nov 76		NUMBER 03		NUMBER MC-AAA-C		CASTING NUMBER WVT. ARS.		PROOF OFFICER W. O. 445-7677-94		Junction		Case Loss, indicated in 1/1000" of inch.	
FIRING STATUS (Check One)		NUMBER OF ROUNDS 47		FIRING STATUS (Check One)		NUMBER OF ROUNDS 47		FIRING STATUS (Check One)		NUMBER OF ROUNDS 47		FIRING STATUS (Check One)		NUMBER OF ROUNDS 47	
BEFORE		AFTER		BEFORE		AFTER		BEFORE		AFTER		BEFORE		AFTER	
hear Face OF Tube				216.90	+0.01	215.00	+0.02	210.00	+0.02	205.00	+0.02	200.00	+0.02	195.00	+0.02
				190.00	+0.02	185.00	+0.01	180.00	+0.01	175.35	+0.00	175.15	+0.00	170.00	+0.00
				165.00	+0.00	160.00	+0.00	155.00	+0.00	150.00	+0.00	145.00	+0.00	140.00	+0.00
				135.00	+0.00	130.00	+0.00	125.00	+0.00	120.00	+0.00	115.00	+0.00	110.00	+0.00
				105.00	+0.00	100.00	+0.00	95.00	+0.00	90.00	+0.00	85.00	+0.00	80.00	+0.00
				75.00	+0.00	70.00	+0.00	65.00	+0.00	60.00	+0.00	55.00	+0.00	50.00	+0.00
				45.00	+0.00	40.00	+0.00	35.00	+0.00	30.00	+0.00	28.00	+0.00	26.00	+0.00
				24.00	+0.00	22.00	+0.00	21.50	+0.00	21.00	+0.00	20.75	+0.00	20.60	+0.00
				Pullover Meas.	20.75"	2.398"	2.395"								
															No basis for estimate of remaining life.

SHEET 2 OF 2

#### SPECIAL MEASUREMENTS

		OPTICAL MEASUREMENTS			
		BASIC	ACTUAL	BASIC	ACTUAL
TOTAL LENGTH OF GUN	-----	-----	-----	ROTATION OF TUBE AT BREECH	-----
TOTAL LENGTH OF TUBE	-----	217.00"	-----	MOVEMENT OF TUBE AT BREECH	-----
DEPTH OF BREECH RECESS	-----	-----	-----	NUMBER OF LANDS AND GROOVES	16 16

Borescoped: (Not chrome plated)

Light scratches, stains, and deposits thru-out chamber. Light smooth erosion encircling centering cylinder beginning 16.10" from rear face of tube (RFT) and continuing forward into main bore to 58" from (RFT). Lands are rounded thru-out eroded area of bore with edges of lands rounded as far forward as 90" from (RFT). Very light longitudinal scoring between 16.10" and 26" from (RFT). Light heat checking encircling bore between 14" and 65" from (RFT). Very light erosion encircling piezo gauge holes. No separation at the junction of the tube and extension was noted.

No photos or impressions taken at this time.

— STAMPED	STARGAUGED AND INSPECTED BY <u>McWILLIAMS</u>	REVIEWED BY
RODMAN <u>GILLEY</u>	TIME —	COMPILATOR
RECORDER <u>SCARBOROUGH</u>	PLACE <u>TRANSONIC RANGE</u>	GRAPHED BY

## MULTIPLE STARGAGE MEASUREMENT &amp; INSPECTION DATA FORM

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SHEET		OF 2		60 MM Tube, MC-AAA				
NUMBER	MODEL	MANUFACTURER	CASTING NUMBER	Muzz. Face of Tube	Rear Face of Tube	GAZE ANGLE, SPANNED	GAZE ANGLE, SPANNED	
60MM TUBE	03	PROOF OFFICER MR. BRANDON	W.O. 445-71677-94	10	216.90	VERT +.001	HOR +.025	
				20	215.00	+.001	+.026	
				7.00	210.00	.000	.000	
				12.00	205.00	-.001		
				17.00	200.00		-.00	
				22.00	195.00			
				27.00	190.00			
				32.00	185.00			
				37.00	180.00			
				Junction	41.65	175.35		
					41.85	175.15		
					47.00	170.00		
					52.00	165.00		
					57.00	160.00		
					62.00	155.00		
					67.00	150.00		
					72.00	145.00		
					77.00	140.00		
					82.00	135.00		
					87.00	130.00		
					92.00	125.00	.000	
					97.00	120.00	000	
					102.00	115.00		
					107.00	110.00		
					112.00	105.00	+.001	
					117.00	100.00		
					122.00	95.00		
					127.00	90.00		
					132.00	85.00		
					137.00	80.00		
	142.00	75.00						
	147.00	70.00						
	152.00	65.00						
	157.00	60.00						
	162.00	55.00						
	167.00	50.00						
	172.00	5.00						
	177.00	40.00						
	182.00	35.00						
	187.00	30.00						
	189.00	28.00						
	191.00	26.00						
	193.00	24.00						
	195.00	22.00						
	195.50	21.50						
	196.00	21.00						
	196.25	20.75						
	196.40	20.60	+.054	+.051				
				+.071				
				+.08				
DATE OF GAUGING	12 MAY 77	PULLOVER DIST	20.75"	VERT 2.414"				
				HOR 2.412"				
NO BASIS FOR ESTIMATE OF REMAINING LIFE.								

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SHEET 2 OF 2

60 MM TUBE, MCAAAC, #03  
12 MAY 77 A.F. 69 RDS.

FOR : MR BRANDON  
W.O. 445-77677-94

Borescoped: Not Chrome Plated

Moderate to light heat checking encircling chamber slope beginning 14" from rear face of tube (RFT) and extending forward into bore to 70" from (RFT). Moderate to light smooth erosion with light traces of scoring encircling centering cylinder beginning 16.10" from (RFT) and extending forward into bore to 23" from (RFT), then becoming light as far forward as 58" from (RFT). Lands rounded thru-out eroded area with driving edge rounded as far forward as 90" from (RFT). Very light erosion encircling plieno gauge holes in bore. No separation was noted between the extension.

No photos or impressions taken at this time.

STAMPED	STARGAUGED AND INSPECTED BY <b>H. BOWERS</b>	REVIEWED BY
RODMAN <b>T. SEARS</b>	TIME —	COMPILATOR
RECORDER <b>M. SCARBOROUGH</b>	PLACE <b>TRANSONIC RANGE</b>	GRAPHED BY

**MULTIPLE STARGAGE MEASUREMENT & INSPECTION DATA FORM**

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SHEET 10F2

60 M/M tube, MC-AAAC

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60 MM Tube MC- AAC				CHAMBER					
DISTANCE (inches) FROM REAR FACE OF BREECH				GAUGE MEASUREMENTS INDICATED IN 1/1000 OF AN INCH					
MUZZLE FACE	REAR FACE OF TUBE	BASIC DIAMETER	ZERO	GAUGE READING	ACTUAL DIAMETER	DIFFERENCE	GAUGE READING	ACTUAL DIAMETER	DIFFERENCE
20.05			2.392	+058	2.450		+064	2.456	
19.00				70	462		75	467	
17.00				87	479		90	482	
16.20				+118	2.510		+121	2.515	
14.00			4.000	+019	4.019		+020	4.020	
12.00				69	69		68	68	
10.00				118	118		118	118	
8.00				166	166		166	166	
6.00				216	216		215	215	
4.00				265	265		265	265	
2.00				314	314		314	314	
1.00				358	338		337	337	
.50				350	350		350	350	
.10				+361	4.361		+361	4.361	
SPECIAL MEASUREMENTS									
TOTAL LENGTH OF GUN	BASIC	ACTUAL	ROTATION OF TUBE AT BREECH				BASIC	ACTUAL	
TOTAL LENGTH OF TUBE	217.00			MOVEMENT OF TUBE AT BREECH					
DEPTH OF BREECH RECESS				NUMBER OF LANDS AND GROOVES				16	16
Borescoped: (Not Chrome Plated)									
<p>Light scratches, stains with moderate to heavy carbon and other deposits thru-out main bore. Moderate to light heat checking encircling chamber slope beginning 14" from rear face of tube (RFT) and extending forward into bore to 85" from (RFT). Heavy to moderate erosion with light longitudinal scoring encircling centering cylinder beginning 16.10" from (RFT) and extending forward into bore to 35" from (RFT), then becoming light as far forward as 115" from (RFT). Light erosion encircling piezo gauge holes in bore. No separation was noted between tube and extension.</p>									
<p>No photos or impressions taken at this time.</p>									
STAMPED		STARGAUGED AND INSPECTED BY				REVIEWED BY			
RODMAN	J. M. WILLIAMS	TIME				COMPILATOR			
RECORDER	I. SEARS	PLACE				GRAPHED BY			

PAGE 1 of 2

**MULTIPLE STARGAGE MEASUREMENT & INSPECTION DATA FORM**

PAGE 2 of 2

60 MM Tube MC-MAC					CHAMBER					
DISTANCE (Inches) FROM			GAUGE MEASUREMENTS INDICATED IN 1/1000 OF AN INCH							
REAR FACE OF BREECH	MUZZLE FACE	REAR FACE OF TUBE	BASIC DIAMETER	ZERO	VERTICAL		HORIZONTAL			
					GAUGE READING	ACTUAL DIAMETER	DIFFERENCE	GAUGE READING	ACTUAL DIAMETER	DIFFERENCE
		20.05		2	+.062	2.454		+.067	2.459	
		19.00		2	.74	.466		.78	.470	
		17.00		2	.90	.482		.94	.486	
		16.20		2	+.121	2.513		+.129	2.521	
		14.00		1	+.020	4.020		+.020	4.020	
		12.00		1	.70	.070		.70	.070	
		10.00		1	.18	.118		.19	.119	
		8.00		1	.67	.167		.67	.167	
		6.00		1	.217	.217		.217	.217	
		4.00		1	.266	.266		.266	.266	
		2.00		1	.315	.315		.315	.315	
		1.00		1	.338	.338		.339	.339	
		.50		1	.352	.352		.352	.352	
		.10		1	+.361	4.361		+.361	4.361	
(cont.) in bore. No separation was noted between tube and extension.										
No photos or impressions taken at this time.										
SPECIAL MEASUREMENTS										
TOTAL LENGTH OF GUN	BASIC	ACTUAL	ROTATION OF TUBE AT BREECH			BASIC	ACTUAL			
	—	—	MOVEMENT OF TUBE AT BREECH			—	—			
	—	217.00	NUMBER OF LANDS AND GROOVES			16	16			
BORESCOPED: (Not Chrome Plated)										
<u>Light scratches, stains, rust and rust pitting with moderate to heavy carbon and other deposits throughout chamber and main bore. Moderate to light heat checking encircling chamber slope beginning 14" from rear face of tube (RFT) and extending forward into bore to 85" from (RFT). Heavy to moderate erosion with light longitudinal scoring encircling centering cylinder beginning 16.10" from (RFT) and extending forward into bore to 99" from (RFT), then becoming light as far forward as 115" from (RFT). Light erosion encircling piezo gauge holes in</u>										
STAMPED	STARGAUGED AND INSPECTED BY O. Tasch			REVIEWED BY (Cont. above)						
RODMAN T. Sears	TIME			COMPILATOR						
RECORDER J. Clark	PLACE Sandy Point			GRAPHED BY						

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